

Simulation Analysis of Cantilever Construction of Extradosed Cable-Stayed Bridge

Jingxian Shi¹ and Yingjie Cheng²

¹ Oxbridge College, Kunming University of Science and Technology, KunMing 650106 Yunnan, China;

² Yunnan Aerospace Engineering Geophysical Detecting Co.Ltd, Kunming 650217, Yunnan, China
sara_shivip@163.com, 532965722@qq.com

Keywords: Extradosed cable-stayed bridge, construction simulation.

Abstract: In the construction of long span beam, the bridge is in linear with the requirement of the design alignment is the key to ensure that the bridge is in a reasonable stress state, the safety of the bridge operation and the beautiful appearance of the bridge. An example of a Extradosed cable-stayed bridge is presented in this paper, a three-dimensional finite element solid model is established by the simulation analysis of Midas software, and the deflection and stress of main girder in each construction stage are simulated and analyzed, the bridge construction process is simulated and calculated as well.

1 INTRODUCTION

The simulation analysis of bridge construction includes: set up a detailed model of each bearing member in the whole bridge range; by using the reliable numerical analysis method, such as the finite element method, the above model is analyzed and calculated, and a relatively detailed and reliable analysis result is obtained; with the help of rich and effective graphic display software, a large number of calculated numbers are visualized, and the distribution images of the calculated results of the displacement, stress and strain of all parts of the whole bridge and each stage are seen directly, analyze and judge directly from the image to obtain useful conclusions and guide the construction in time. The bridge structure simulation is built up and improved with the development of finite element technology and computer software and hardware.

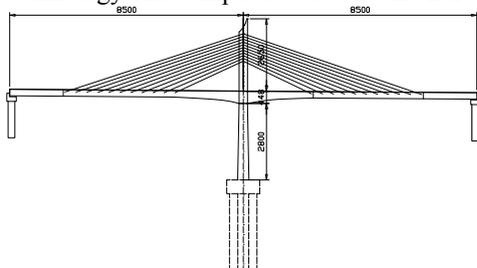


Figure 1: Bridge longitudinal section diagram

In this paper, A 2X175m Extradosed cable-stayed bridge as an example. The main beam is a single box three chamber large cantilever variable cross section PC continuous box girder. the height of the fulcrum beam and middle beam are 4.48m and 2.85m respectively, box beam top width 27m, the length of cantilever flange plate is 4.5m. Reinforced concrete single column solid rectangular cross section in main tower, which the height of tower is 26.5m. The cable-stayed is arranged on the central partition with 11 pairs of 44 rows; tower and beam are consolidated together. design load: Road- II , crowd load-3.5kN/m²; bridge width- 27m.

2 CONSTRUCTION SIMULATION ANALYSIS

The cantilever construction stage of the main bridge box girder is the key and difficult point of the whole bridge construction, the construction of each beam can be decomposed into 6 construction steps: basket moving forward; adjustment the elevation of the mould plate; concrete pouring; tensioning prestress; Preliminary tensioned stayed cable(with cable section); precise adjustment of stayed cable (with cable section). The division of the main beam segment is shown in Figure 2.

Table 3 Construction stage division of calculation model

construction stage	Name of construction component	Working condition description
1	Pier	Bridge pier construction
2	0#block	Pouring 0# block concrete and tensioning prestress
3	Bridge tower	Bridge tower construction
4-6	1#beam	Install the basket-Concrete pouring-Forming beam section-Tensioning prestress
7-18	2#beam-5#beam	Basket moving forward-Concrete pouring-Forming beam section-Prestressed steel bundles in each section of tensioned beam
19-62	6#beam-16#beam	Basket moving forward-Concrete pouring-Forming beam section-Prestressed steel bundles in each section of tensioned beam-stayed cable on a tensile beam
63-65	17#beam	Basket moving forward-Concrete pouring-Forming beam section-Tensioning prestress
66	Side span cast-in-place section	Full framing construction
67-69	Closure section	Cradle at both ends of the closure-Exerting weight at both ends of the closure-Installation of skeleton
70-71		Pouring concrete of closure section-Remove the weight simultaneously-Closure section to form beam section
72-81		Tensioned baseplate continuous steel beam-Tensioned roof continuous steel beam
82-84		Dismantling the cradle of the closing section-Dismantling the basket of 16# beam-Dismantling the side span of the cast-in-place full framing
85	The second phase	Secondary dead load
86	Completion	Working condition of completed bridge
87-88	Operation	Operation stage (10years) ,Operation stage (30years)

Table 4: Cable force

Cable number	Designed cable force/kN
West1-West3 East1-East3	3150
West4-West6 East4-East6	3400
West7-West11 East7-East11	3650

2.4 Calculation of load parameters

1) The main beam unit has input $\gamma=26\text{kN/m}^3$ in the material characteristics, and has calculated the area in the section characteristics. Therefore, the calculation of dead load weight is automatically counted. Manually add concrete wet weight and diaphragm weight. The beam is exerted in the form of a concentrated force at the forming stage.

2) secondary dead load: bridge deck pavement $q_1=66.36\text{ kN/m}$; Crash barrier of edge $q_2=12.43\text{ kN/m}$; Middle collision guardrail $q_3=16.30\text{ kN/m}$; Sidewalk $q_4=25.37\text{ kN/m}$; Total: $q = 120.46\text{kN/m}$.

3) The specific value of cable force in stayed cables is shown in Table 4

4) In the checking calculation, the data are input according to the parameters of the design diagram. The pre-stressed reinforcement adopts 9 beams and 12 beams of $\phi 15.24$ steel strands, $f_{pk}=1860\text{MPa}$, Anchorage deformation is 6mm, Deviation factors of pipeline is 0.0015. The other related parameters for the calculation of the pre-stressed are shown in Table 5.

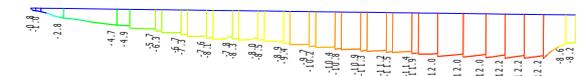
Table 5: Physical parameters of pre-stressed reinforcement

The number of physical types of steel beam	1	2
Steel beam model	15—9	15—12
Pipe diameter/m	0.087	0.103
Steel area/m ²	0.00126	0.00238
Tension stress/MPa	1395	1395
coefficient of relaxation	0.3	0.3
coefficient of friction resistance	0.25	0.25

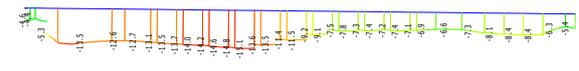
5) The coefficient of shrinkage and creep is calculated by the program according to the current highway bridge design code, and 3000 days after the complete is calculated. The temperature influence is mainly considered as follows: The system has a uniform rise and fall of 20 °C ; The temperature gradient of the tower section is ± 5 ; The temperature of the cable and tower are ± 10 °C . Support settlement is calculated by 0.02M.

6) The vehicle live load is bi-directional 4 lane, the reduction coefficient is 0.67, and the highway - II grade. The impact coefficient is automatically calculated by program. The load of the crowd is calculated according to the 3.5kN/m², and the other loads are calculated according to the standard.

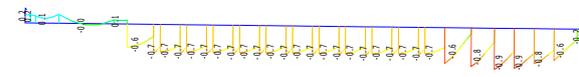
the section safety factors of pier bottom and tower bottom are 5.03 and 2.17 respectively, and all are in a safe state.



(A) Compression stress envelope of the upper edge of the main beam (half bridge)



(B) Compression stress envelope of the lower edge of the main beam (half bridge)



(C) The tensile stress envelope of the upper edge of the main beam (half bridge)



(D) The tensile stress envelope of the lower edge of the main beam (half bridge)

Figure 4: Calculation result of main beam stress

3 ANALYSIS RESULT

3.1 Stress checking of the main beam

According to the 7.2.8 provision of <code for design of highway reinforced concrete and pre-stressed concrete bridges and culverts>(JTG D62-2004), the limit value of compressive stress of the main beam in construction stage is $0.729.6=20.72\text{MPa}$ and the tensile stress limit value is $1.15\times 2.51=2.8865\text{MPa}$. According to the results of simulation analysis, the stress envelope diagram of main beam in all stages of construction is shown in Figure 4, the maximum compressive stress and the maximum tensile stress are 15.1MPa and 0.9MPa respectively, which all meet the specification requirements

According to the above length calculation, the bridge pier tower is in the safe state. The maximum cantilever phase safety factor of tower bottom section is 2.60; under the special condition of wind,

3.2 Checking calculation of stayed cable force

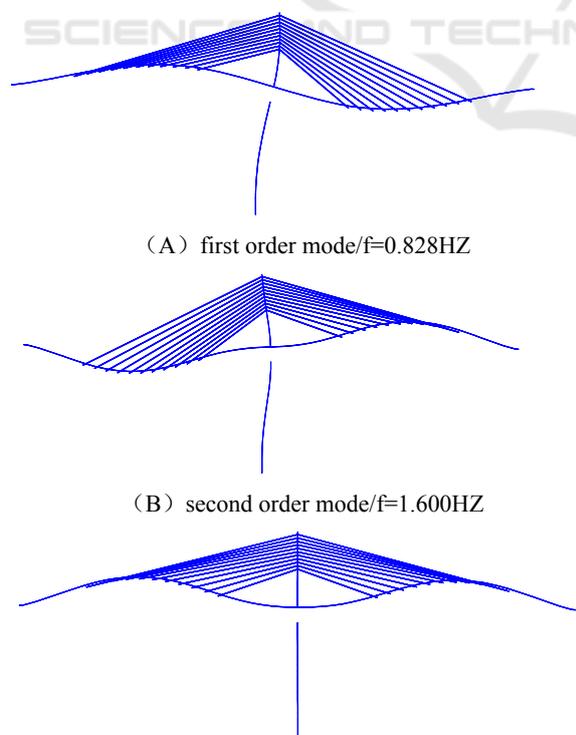
According to the results of the monitoring and calculation, the safety factor of the stayed cable at whole construction process is more than 2. and the minimum safety factor is all up to the specification requirements.

Table 6: Calculation result of stayed cable force in construction stage

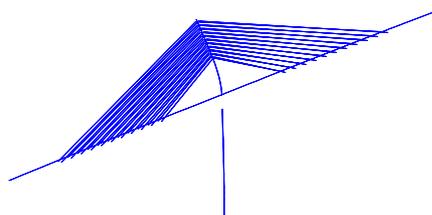
cable number	Number of steel beam	safety factor
West1、 East1	31	2.47
West2、 East2	31	2.46
West3、 East3	31	2.43
West4、 East4	34	2.45
West5、 East5	34	2.42
West6、 East6	34	2.40
West7、 East7	37	2.42
West8、 East8	37	2.40
West9、 East9	37	2.39
West10、 East10	37	2.37
West11、 East11	37	2.37

3.3 Frequency and mode of vibration

The 20 order modes of vibration is calculated in this paper. The results of the first 4 order frequencies and modes of vibration are shown in Figure 5



(C) third order mode/f=1.773HZ



(D) fourth order mode/f=2.969HZ

Figure 5: Modes and frequencies of each order.

4 CONCLUSIONS

Combining with the engineering example of 2X175m Extradosed cable-stayed bridge , the simulation analysis of cantilever construction of the bridge is mainly done. The parameter selection, model establishment, construction stage division and operation result analysis of the construction simulation for the Extradosed cable-stayed bridge are expounded. The theoretical basis is provided to ensure The linear shape of the bridge. and stress of the bridge, and provide reliable technical guarantee for the safety construction of the bridge.

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